Steels for larger forged parts Ouality Instructions

STAHL-EISEN-WERKSTOFFBLATT 550 3rd Edition

The sections marked with a dot (•) contain information about the agreements to be made for an order or which can be made.

1. Scope

- 1.1 This material data sheet covers steels, which are used in a heat-treated or normalized condition for larger open die forged construction parts also at higher temperatures (please see also section 7.4). 1)
- 1.1.1 For the scope regarding the used cross section to be taken into consideration this material data sheet is in relation to DIN 17 100 heat-treatable steels.

For limiting the scope further the following data sheets must be stated:

SEW 555 (Stahl-Eisen-Werkstoffblatt) – steels for larger forged parts as construction parts of turbines and generator plants – (in future):

SEW 089 Part 6 (Stahl-Eisen-Werkstoffblatt) – forged parts of fine grain construction steels suitable for welding – (in preparation);

SEW 620 (Stahl-Eisen-Werkstoffblatt) – forged parts of heat-resistant steels suitable for welding – (new issue in preparation);

SEW 640 (Stahl-Eisen-Werkstoffblatt) – steels for parts in the primary circuit of nuclear power plants -;

SEW 640 (Stahl-Eisen-Werkstoffblatt Addendum 1 – steels for nuts and bolts for the use at slightly higher temperatures as construction parts in the primary circuit of nuclear power plants – (in preparation).

2. Denominations

Steels for larger forged parts are heat-treatable steels with cross sections taken into consideration and chemical compositions corresponding to the requirements.

3. Dimensions and allowable dimension deviations

• The dimensions and the admissible dimension deviations must be agreed upon when ordering.

4. Weight calculation and allowable weight deviations

- 4.1 For calculating the nominal weight of a forged part from steels according to this material data sheet a densitiy of 7.85 kg/dm³ is assumed.
- 4.2 The admissible weight deviations can be agreed upon when ordering.
- 1) The preceding issue of the SEW 550 (Stahl-Eisen-Werkstoffblatt) (of 1957) covers a relatively large number of steel grades for forged parts of various types and for different applications; e.g. including those for the turbine and generator industry. It has proven to be recommendable, to cover the steel qualities required for these construction parts in a special date sheet (SEW 555). The existing issue of he SEW 550 therefore contains only those steel grades, which are used for more general applications such as for the machine tool industry and which are partly similar to the standard heat-treatable steels.

Page 2 SEW 550 (Stahl-Eisen-Werkstoffblatt)

5. Grade classification and steel selection

- 5.1 This material data sheet covers the steel qualities as stated in table1. They are principally classified according to the chemical composition and are killed. These steels are special steels.
- 5.2 Selecting the steel quality is the responsibility of the buyer. It is recommended to ask the producer for assistance.

6. Denomination

The short names for the steel grades are in correspondence with section 2.1.2 of the explanatory comments to the standard book 3, the Werkstoff-Nos. are determined according to DIN 17 007 sheet 2.

7. Requirements

- 7.1 Method of Melting
 - The producer decides on the method of melting and desoxidation as long as nothing else
 has been agreed upon when ordering.
 The method of melting must be made known to the buyer on request.
- 7.2 Supply condition
- 7.2.1 Normally the forged parts are supplied in a condition finish heat-treated, machined according to the details as stated in the drawings
- 7.2.1.1. The type of heat-treatment to achieve the guaranteed properties is at the discretion of the producer; it must be stated on request of the buyer.
- 7.2.21. Normally the forged parts must be supplied separated according to heats.

7.3. Chemical composition

- For the chemical composition as per melt analysis table 1 applies. Deviations from the composition limits as stated in table 1 are allowed as long as the guaranteed properties are not influenced negatively. In special cases an agreement about the deviations must be reached with the buyer.
- 7.4. For the forged parts the values for the mechanical properties as stated in tables 2 4 are guaranteed.
- 7.4.1.1 The following cross section shapes and dimensions can e used as near equivalents to the governing diameters for the heat-treatment 2) (see tables 2-4):
 - a) for cylindrical solid parts the diameter;
 - b) for non-cylindrical solid parts factor 1.5 of the smallest corner length
 - c) for open cylindrical hollow bodies:
 - 2 times of the wall thickness, if the interior diameter is smaller than 80 mm
 - 1.75 times of the wall thickness, if the interior diameter is between 80 and 200
 - 1.5 times of the wall thickness, if the interior diameter is more than 200 mm

- d) for closed cylindrical hollow bodies -2.5 times of the wall thickness
- e) for non-cylindrical hollow bodies the governing diameter for the heat-treatment must be judged analogously according to section c) or d).
- The indication of certain limits for the governing diameter for the heat-treatment 7.4.1.2 does not mean, that the corresponding forged parts can be through heat-treated down to the core. If such a condition of a forged part is demanded the producer must be informed and an understanding about the suitable steel quality must be reached between the buyer and the producer or – if necessary – a special agreement must be made.
- An overview about the minimum values of the yield strength at room 7.4.2 temperature in relation to areas of the governing diameter for the heat-treatment is given in table 5^3) as an indication for the application.

Technological Properties 7.5.

Suitability for welding

The steels according to this data sheet can only be welded under consideration of the for the quality individually required measures. In case welding is done by the producer a consultation with the customer is recommended.

For welding of constructions the steel grades Ck 22, 20 Mn 5, 28 Mn 6, 20 MnMoNi 4 5, NiMoCr 4 7, 24 CrMo 5 are to be preferred.

Physical Properties 7.6.

The (dynamic) modulus of elasticity of the steels changes with the temperature 7.6.1. approximately as follows 4)5):

at	20°C	100°C	200°C	300°C	400°C	(500°C)	(600°C)
10 ³ N/mm ²	212	207	200	193	184	(175)	(164)

The medium linear coefficient of thermal expansion is approximately 4)5) 7.6.2

between	20°C and	100°C	200°C	300°C	400°C	(500°C)	(600°C)
10 ⁻⁶	K ⁻¹	12.5	13.2	13.7	14.2	(14.6)	(14.9)

²⁾ for this and other technical expression of the heat treatment see DIN 17 014 sheet 1

³⁾ table 5 see page 5

⁴⁾ These are medium (average) values of values measured at steels according to this technical data sheet and other comparable steels after examinations in the near past; the values measured at various steels can be averaged because the property values in relation to the covered steel qualities fluctuate only insignificantly. See in this respect especially the following publications: Fink, K., F. Richter, U. Lotter u. K. Schrecke: Thyssen-Research. 2 (1970) S. 65/80: Richter, F: The most important physical properties of 52 iron qualities, Steel Iron special report copy 8, Düsseldorf 1973.

⁵⁾ With regard to the scope of this technical data sheet the values for 500°C and 600°C are stated in brackets.

7.7. Condition at the surface and within the interior

- 7.7.1. The forged parts must be free of any defects which might influence their application negatively more than normal.
- 7.7.2. The parts supplied in non-machined condition should have a smooth surface as well as the modern forging technology allows.
- 7.7.2.1. Within the machining allowance surface defects are allowed and can be removed as long as the application of the product is not influenced in a negative way.
- 7.7.3. Repairs of defects by welding required the approval of the buyer or his representative.
- 8. Tests
- 8.1 **Delivery tests**
 - For orders of forgings from the steels acc. to this technical data sheet delivery tests can be agreed upon, which normally are carried out by experts of the supplying mill but also as per special agreement by external representatives of the buyer.
- 8.2 Heat treatment condition at the test
- 8.2.1. The parts are normally tested in the heat treatment condition, for which the guaranteed mechanical properties are stated in tables 2 to 4.
- 8.2.2. A test in other heat-treatment conditions, taking samples from the piece before the heat-treatment and their seperate and/or special heat-treatment must be especially agreed upon when ordering
- 8.3 **Scope of testing**
- 8.3.1 test units
- 8.3.1.1 The forged parts should be tested separated by heat numbers and heat-treatment lots.
- 8.3.1.2. Forged parts with similar dimensions and similar forging ratio from the same heat and the same heat-treatment lot are combined into one testing unit. In case the total weight of the pieces of such a testing unit is less than 10 tons one piece will be tested; in case of a larger total weight two pieces are tested.
- in all other cases the size of the testing units and the number of pieces of the testing units to be tested will be chosen by the producer accordingly as long as there are no other agreements when ordering.

- 8.3.1.2.2. If in other so far valid supply instructions more comprehensive testing units and/or smaller numbers of pieces to be tested per testing unit are stated compared with the ones stated in section 8.3.1.2, then these instructions should remain valid.
- 8.3.1.3. It must be stated in the order if each piece should be tested individually.
- 8.3.2. Tests to be executed and number of samples
- 8.3.2.1. From parts for testing as per sections 8.3.1.2 to 8.3.1.3 normally one sample each must be taken for the tensile test and 3 samples for the notch impact-bending test.
- 8.3.2.2. In case no testing of the tensile strength and no notch impact-bending test is considered or the taking of samples is impossible then a hardness test can be done. The hardness values to be observed in that case must be agreed upon.
- 8.3.2.3. If the yield strength at increased temperature should be examined this must be be stated explicitly in the order sheet. The yield strength might be checked only at one sample and only at one temperature above room temperature (within the temperature range as per table 4). The testing temperature must be indicated in the order sheet.
- 8.3.2.4. A non-destructive test (e.g. ultrasonic test or as per the electromagnetic method) must be agreed upon when ordering.

8.4. Sample taking

- 8.4.1. The samples in sufficient number of pieces must be taken either directly from the part or an additional allowance for the samples in sufficient lengths must be given.
 - At the forged parts material for the samples for repeat tests and in case this has been agreed upon when ordering sample material for tests of the buyer must be given.
- 8.4.2. When taking samples for tensile tests and notched-bar tests a difference must be made between their geometric location in the part and their position in relation to the grain flow.
- 8.4.2.1. The acronyms L,T,Q used in tables 2 and 3 name the position of the samples in relation to the grain flow and must be understood within this technical data sheet as follows:
 - L: the longitudinal axle of the sample is parallel to the general stretch direction of a non-curved grain flow
 - T: the longitudinal axle of the sample cuts a curved grain flow as a type of chord (and thus takes a certain 'sloping position' to the grain flow)
 - Q: the longitudinal axle of the sample cuts a curved or non-curved grain flow vertically

Samples with their longitudinal axle in direction of an additional up-setting (vertically to it's width) of the grain flow (so called sample location in 'thickness direction') do not fall under the sample position marked as Q (see section 8.4.2.1.2)

- In case of doubt the sample taking with regard to their position to the grain flow and under consideration of these instructions must be agreed upon when ordering. If there are no agreements the position of the samples with regard to the grain fow will be determined by the producer.
- Taking samples of which the longitudinal goes through a spread grain flow vertically to the broadening (in thickness direction), must be agreed upon especially when ordering whereas the minimum values to be observed must be determined especially of the toughness values.
- When ordering the position of the samples in relation to the geometry of the part which might be important for the mechanical load can be agreed upon. In this case it must be checked, though, whether and to what extent the guaranteed values of the mechanical properties stated in tables 2 and 3 especially the minimum toughness values set with regard to the grain flow correspond to those requirements. If necessary the values of the mechanical properties to be guaranteed must be agreed upon in such cases.
- 8.4.3. For the sample taking location within the cross section the following applies:

The samples must be taken from the cross section area between the surface and 1/6 of the diameter or the (wall) thickness and maybe in a corresponding distance from another, neighbouring surface.

• If another location for the taking of the samples in the cross section must be considered then this must be agreed upon in the order sheet; the values of the mechanical properties to be guaranteed must also be determined.

8.5. Test methods to be applied

- 8.5.1. The chemical composition is to be determined according to the method set by the Committee of the Chemical Engineers of the Association of German Ironworks Experts ⁶⁾. Methods not set by the Committee must be especially agreed upon.
- 8.5.2. The tensile test must be executed according to DIN 50145. Normally a short proportional test bar (with the measuring length $L_o = 5 d_o$) according to DIN 50 125 should be used; the result determined with this bar is decisive in arbitration cases.
- 8.5.2.1. If the yield point is cannot be clearly determined then the 0.2 % yield strength must be identified.
- 8.5.3. The hardness test must be executed according to DIN 50103 (hardness test acc. to Rockwell), DIN 50133 (hardness test acc. to Vickers) or DIN 50351 (hardness test acc. to Brinell).
- 8.5.4. The notched bar test must be executed acc. to DIN 50115 at DVM-samples.
- 8.5.4.1. The impact value is to be determined as average from 3 tests at samples, which are positioned always side by side in the same distances from the surface or in case this is impossible or does not make sense directly one after the other in the same part.
- 8.5.5. For non-destructive tests the method to be used must be agreed upon when ordering.

8.6. Repeat tests

- 8.6.1. If the insufficient result of a test is obviously due to defects in the testing technology or a closely limited defect spot of a sample then the wrong result must not be considered for the decision about meeting the requirements and the corresponding test must be repeated.
- 8.6.2. If the results of a correct test are insufficient for the requirements set a repeat test can be done which normally means two more tests at the same sample for each insufficient test result.

The part is to be considered to meet the conditions if both repeat tests are satisfactory. It can be rejected if one of the two repeat tests are insufficient.

8.6.3. If the reason for an insufficient test can be removed by a corresponding heat-treatment then the part can be heat-treated again after which the test must be repeated.

8.7. Test certificates

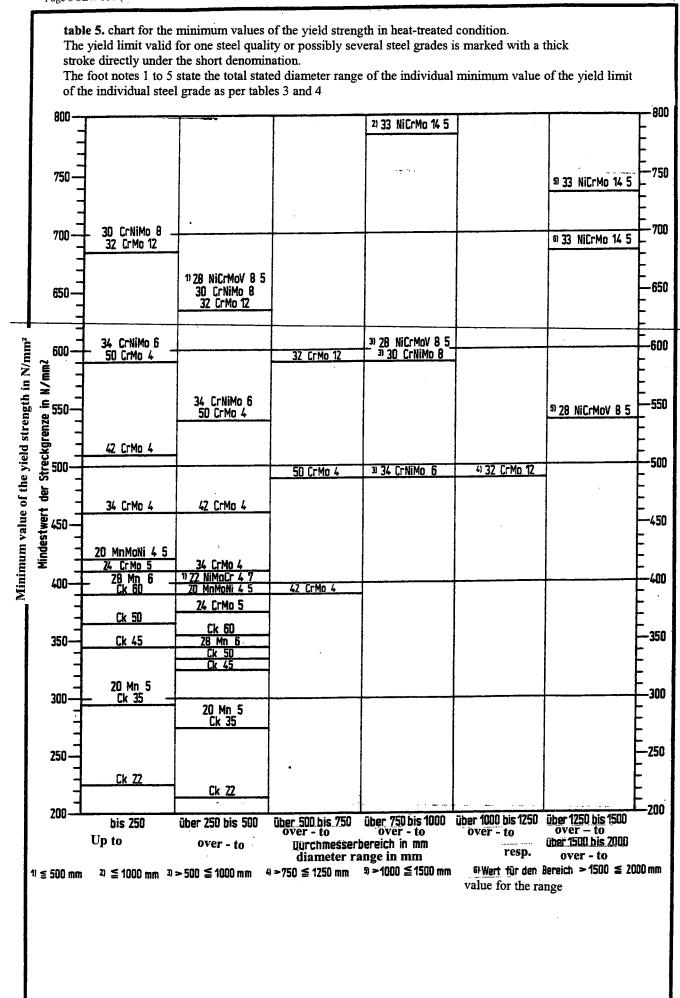
• The delivery test is certified by a certificate according to DIN 50 049. The type of the certificate is to be agreed upon when ordering.

9. Claims $^{7)}$

- 9.1 External and interior defects can only be claimed if they considerably influence the steel quality and the type of the forged part and its application negatively.
- 9.2. The buyer must allow the supplying mill within a reasonable time limit to convince themselves that the claim is justified; as much as possible by providing the claimed part and reference samples of the quality supplied.

⁶⁾ Manual for the Iron Works Laboratory, volume 2; The examination of metallurgical material; volume 4: arbitration analysis, volume 5: additional volume; Düsseldorf, Verlag Stahleisen mbH, always the latest valid issue.

⁷⁾ Explanations regarding this claim clause in quality standards for iron and steel see DIN-publication 40 (1961) page 111/122



> %

Ź%

0,50/0,80 0,15/0,30 0,45/0,60 0,20/0,35 0,15/0,30 0,16/0,30 % Mo 0,30/0,50 0,30/0,50 0,90/1,20 0,90/1,20 0,90/1,20 0,90/1,20 2,80/3,30 ≥ 0,50 <u>ن</u> % Chemical composition 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,035 maximum % • 0,035 0,035 0,036 0,036 0,035 0,035 0,035 0,035 0,035 0,035 0,035 0,036 Table 1. Chemical composition of the steel grades for larger forged parts 0,60/0,80 1,30/1,65 1,00/1,30 0,30/0,60 0,50/0,80 06'0/09'0 06'0/09'0 0,50/1,00 1,00/1,50 0,60/0,80 0,50/0,80 0,40/0,70 % Mu 0,50/0,80 0,50/0,80 Tafel 1. Chemische Zusammensetzung der Stähle für größere Schmiedestücke 09'0/06'0 ≥ 0,36 ≥ 0,35 ≦ 0,40 96,0 ≧ ≥ 0,35 ≤ 0,40 % % ≤ 0,40 ≤ 0,40 ≦ 0,40 ≦ 0,40 ≤ 0,40 ≦ 0,40 0,18/0,26 0,47/0,55 0,32/0,39 0,42/0,50 0,30/0,37 0,28/0,35 39'0/49'0 0,17/0,23 0,17/0,23 0,25/0,32 0,17/0,27 0,20/0,28 0,38/0,45 0,46/0,54 ပ % short name |DIN-Wno. 1.6755 1.1181 1.1191 1.1208 1.1133 1.1170 1.6311 1.1221 1.7220 1.7225 1.7228 1.7381 steel grade 20 MnMoNi 4 5 22 NiMoCr 4 7 34 CrNiMo 6 30 CrNiMo 8 32 CrMo 12 24 CrMo 5 34 CrMo 4 42 CrMo 4 50 CrMo 4 20 Mn 5 28 Mn 6 Ck 45 Ck 22 Ck 38 Ck 50 Ç Ç

•

9'0 ≅ 90'0 ≶ ≥ 0,60

9'0 ≅

0,40/0,801 0,60/1,203

For larger cross sections a Ni-content of up to 1.00 % is allowed -2) for larger cross sections a Ni- content of up to 1.50 % is allowed

≦ 0,15

1,80/2,10 3,20/4,00

0,35/0,55

1,00/1,50

0,035

0,035

0,20/0,60

09'0/06'0

≤ 0,40 ≦ 0,40

0,28/0,36

0,24/0,32

1.6932 1.6956

0,035

1,00/1,70

09'0/06'0

1,80/2,20 1,40/1,70

0,30/0,50

1,80/2,20

1,40/1,70

0,035

0,035

0,40/0,70 09'0/06'0

≦ 0,40 ≤ 0,40

0,26/0,33

0,30/0,38

1.6582 1.6580

0,035

0,15/0,30

≤ 0,15

Table 2. Guaranteed values of the mechanical properties at 20° C for forged parts from non-alloyed steel grades in normalized condition

steel	steel grade	governing	yield point	tensile strength	elongs	elongation $(L_0 = 5 d_0)$	(°p)	impac	impact test (DVM-samples)	-samples)
short name	DIN-Wno.	heat-treatment ¹⁾			the g	sample location in relation to the grain flow ³⁾	lation to	sample le the g	sample location in relation to the grain flow ³⁾	ation to
		Ē	strength ²⁾	N/mm²	J	T % min.	σ	۔۔	J, min.	σ
Ck 22	1.1161	VI	226	410 bis 520	26	23	9	48	14	34
			215	410 bis 520	3 2	21	17	4	34	27
		> 500 ≤ 1000	206	410 bis 520	24	20	9	38	91	24
Ck 36	1.1181	V	276	490 bis 610	55	9	5	38	9	24
			266	490 bie 610	24	12	4	34	22	
		> 500 ≤ 1000	245	490 bis 610	20	91	12	31	. \$	12
;										
\$	1.1191	VII .	326	590 bis 720	81	4	12	31	24	17
			306	690 bis 720	16	6	F	27	21	4
		> 500 ≤ 1000	296	. 590 bis 720	5	12	ô	24	17	4
Ck 60	1.1206	5	345	620 bis 770	Œ	Ē	7	ı		
		> 250 ≤ 500	326	620 bis 770	5	5	: 9	,	۱ ۱	• •
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1) 500 500 (1	S T T T T T T T T T T T T T T T T T T T									

see sections 7.4.1.1 and 7.4.1.2 the 0.2% yield strength is only important in case of an unclear yield point see sections 8.4.2 to 8.4.2.2

Table 3. Guaranteed values of the mechanical properties at 20°C for heat-treated forged parts

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-samples)	lation to	0	_		\$ 6	ī	27	24	,	12	4	ļ	l 1		,	,		2		•	5	5 5			5 2	1	24		2.7	27		57 	24
impact test (DVM-samples)	sample location in relation to the grain flow ³⁾	-	J. min.	AE	34		34	31	-	4 4	5	ı			ı	,		č	34		27				9 8	:	34		4	34		5 7	ē
impact	sample lo the gr		•	5.	. 4		- 41	38	č	26	ì	1	ı		1	,		48	. 6		4	4			÷ 4		4	4	P	48	*	; ;	-
5 d ₀)	elation to	o		19	17		16	4	ç		:	=	0		₽	6		15	4		12	13		3	. 4	!	<u>۔۔۔۔۔</u>	ç	2	7	÷	: \$	<u> </u>
elongation ($\mathbf{L}_0 = 5 \mathbf{d}_0$)	sample location in relation to the grain flow ³⁾	-	% min.	23	2		e	9	ţ	4		14	13	,	2	5		9	18		5	92		4	. 1 0	,	<u> </u>	ň	2	9	6	2 \$	<u>.</u>
elong	sample the			28	52	(77	21	6	17		17	9	¥	₽	4		55	21		6	19		12	- 4	•	2	17	: ;	8	15	<u> </u>	?
tensile strength			Nam	410 bis 540	410 bis 540	400 Lin 0.40	480 DIS 040	480 DIB 640	590 bis 740	690 bis 740		630 bie 780	630 bis 780	600 his 840	Otto sin oso	690 bis 840		490 bis 640	490 bis 640		590 bis 740	540 bis 690	-	580 bis 730	550 bis 700	600 Li	01.800	640 bis 790		080 DIS 740	690 bis 840	640 his 790	
yield point	0.2% yield	N/ms mgm	IV/MM² mm.	226	216	206	376		345	326		990	336	380	9 9 6	200		082	275		080	D 40		420	390	400	•	410	376	3	460	410	
governing diameter for the	heat-treatment ¹⁾	1			> 250 ≤ 500	> 250	> 250 < 500			> 250 ≤ 500				≥ 260	> 950 < 500	- 1			> 260 ≤ 600	9	002 (1 020 /			≥ 560	> 250 ≤ 500	200		≥ 260	> 250 < 500 ·		≥ 260	> 250 ≤ 500	
	DIN-Wno. 7 he			1,1161	^	1.1181		•	1.1191	^		1.1208	^	1.1221			1100			1 1120	-	•		1.6911	^	1.6755		1.7258	^		1.7220	^	
steel grade	short name			3		Ck 35		-	Ck 46			8		Ck 60	-		20 Ma 5)		28 Ma 6	,	£		20 MnMoNi 4 6		22 NiMoCr 4 7		24 CrMo 6			34 CrMo 4		

2 2 2	444 4477	12 2 2 2 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4 4	2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2 2
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8 8 8	2 2 2 4 4 2 2	222 888	14 4 60 60 40 40 40 40 40 40 40 40 40 40 40 40 40
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610 460 390	690 695 690 690 690	685 635 685 695	636 690 640 786 736
A 260 50 600	1	1	AI A
× 260 × 600	> 250 > 260 > 260 > 260 > 750	× × × × × × × × × × × × × × × × × × ×	> 500 > 1000 > 1000 > 1500
1.7226	1.7228	1.6582	1.6932
42 CrMo 4	50 CrMo 4 32 CrMo 12	34 CrNiMo 6 30 CrNiMo 8	28 NICrMoV 8 6 33 NICrMo 14 6

... In case the stated mechanical values for a range of larger heat-treatment diameters should be guaranteed for a dimension from a smaller heat-treatment diameters then this must be agreed upon when ordering. See sections 7.4.1.1. and 7.4.1.2. − 3) the 0.2% yield strength is only important in case of an unclear yield point

see sections 8.4.2. to 8.4.2.2

Table 4. Guaranteed values for the high-temperature yield point of the steel grades in heat-treated condition in correspondence to table 31) 450°C (280) (294)(265) (216) 350°C | 400°C (98) 324 309 274 294 255 206 196 81 108 108 108 226 206 266 231 206 196 177 266 235 343 324 275 33B 294 300°C 0.2% yield strength²⁾ 147 137 123 236 226 256 235 96 98 284 265 226 216 294 255 353 314 N/mm², minimum 363 343 294 yield point or 260°C 216 208 177 167 152 256 245 284 266 304 276 235 226 314 333 363 371 314 200°C 196 186 172 236 216 284 265 304 276 265 246 324 294 333 392 343 363 382 333 100°C 265 245 314 284 211 201 186 333 358 324 280 363 324 407 372 397 358 20°C 225 215 205 295 275 345 325 386 410 375 390 296 276 390 420 390 9 diameter for the heat-treatment¹⁾ 250% 260% 2 500% 260 600 260 250 500 250 500 250 500 250 250 500 600 250 V() Vi Vī VI VII VII VII VII VII VII VII VII Ē > 250 > 260 > 260 > 250 > 250 > 250 > 260 > 250 > 250 DIN-Wno. 1.1161 1.1206 1.1181 1.1191 1.1221 1.1170 1.6311 1.6755 1.7258 steel grade short name 20 MnMoNi 4 5 22 NiMoCr 4 7 24 CrMo 5 20 Mn 5 28 Mn 6 Ck 22 Ck 36 Ck 45 Ck 50 Ç 80

-		266 (235)	363	324	245	20	- 5	294	200	461	412	363	37.1	353	343			392	431	302	363	626	520	471	
-	333	294	392	363	276	410	606	333	236	200	461	392	412	382	363	620	471	431	471	431	402	208	699	610	
-	363	314	422	382	304	451	431	371	679	639	490	422	441	412	382	228	510	471	610	47.1	431	647	598	649	
_	392	343	441	402	324	490	461	402	909	699	510	441	481	461	422	298	549	900	649	200	461	677	628	629	
_	422	371	461	412	333	520	481	431	628	679	630	451	610	471	441	628	629	230	679	530	490	902	667	808	
	441	392	486	431	363	564	510	461	657	808	699	471	648	909	466	657	809	699	809	699	515	746	969	647	
_	460	410	610	460	380	9	540	490	982	635	280	490	280	640	480	685	635	069	636	280	640	765	735	989	
	≥ 250	≥ 200	≥ 250	≥ 500	•		_	≥ 760			≥ 750		≥ 250	§ 500	≥ 1000	≥ 260	≥ 600	≥ 1000		≤ 1000		≥ 1000	V		
_		> 260		> 260	> 600		> 250	> 600		> 250	> 500	> 760		> 260	^ 200		> 260	> 600		> 600	> 1000		v 100D	> 1600	
	1.7220		1.7226			1.7228			1.7361				1.6582			1.6580			1.6932			1.6958			
	34 CrMo 4		42 CrMo 4			50 CrMo 4			32 CrMo 12				34 CrNiMo 6			30 CrNiMo B			28 NIC:MoV 8 5			33 NiCrMo 14 5			

diameters then this must be agreed upon when ordering. 2) See sections 7.4.1.1. and 7.4.1.2. - 3) the 0.2% yield strength is only important in case of an unclear yield point -4) A value in brackets mean, that this steel grade is not provided for this application (and a test) at this temperature. - 5) The values in this line • In case the stated mechanical values for a range of larger heat-treatment diameters should be guaranteed for a dimension from a smaller heat-treatment are valid also for the normalized condition (see table 2) -) The values in this line are valid only for the normalized condition (compare with table 2).

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